#### SAKE ENGINEERS, INC.

## **Engineering - Surveying - Land Development**

400 S. Ramona Ave. Suite 202, Corona, CA 92879

Tel (951) 279-4041

Fax (951) 279-2830

# FINAL HYDROLOGY AND HYDRAULIC REPORT

For

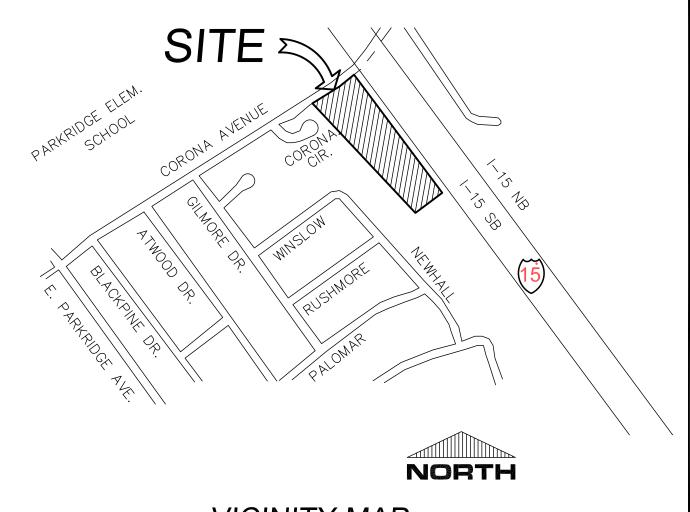
TTM 36864 ON CORONA AVE @ I-15 APN 122-180-027 CORONA, CALIFORNIA

## **Prepared For:**

FATHI MANASRAH, P.E. AL-WAAFA FAMILY TRUST 9319 ALTA CRESTA AVENUE RIVERSIDE, CA 92508 (951) 581-2330

> May 2023 Job No. 3360





VICINITY MAP

NTS

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Rainfall for Corona NOAA Atlas 14 Soil Map Plate C-1.14 Pre-development Hydrology Map Post-development Hydrology Map

### INTRODUCTION

The purpose of this report is to document hydrology and hydraulic calculations for the development of Tentative Tract Map 36864 on Corona Ave at I-15 in City of Corona, CA (APN 122-180-027)

This development consists of total area of 2.1 ac.

Riverside County Flood Control & Water Conservation District (RCFC&WCD) Hydrology Manual methods are used in these calculations.

### PRE-DEVELOPMENT CONDITION

The project site is vacant. The site is sloping from South to North with highest point at 619 feet above mean sea level and lowest point at Corona Ave at elevation of 600.

Existing slope along the 15 freeway will be conveyed via a brow ditch to a parkway drain to Corona Ave.

## **PROJECT OFFSITE**

Storm runoff from the slopes of I-15 freeway enter the project site from the East. The project proposes a lined ditch to receive and convey the runoff before entering the project site.

## **POST-DEVELOPMENT CONDITION**

The proposed project subdivides the parcel into 7 lots of about 1/5 Ac with private street access to Corona Circle.

#### PEAK RUNOFF (CFS)

	I	EXISTIN		DEVELPED			
AREA (Ac)	$Q_{10}$	$Q_{100}$	% PRVS	$Q_{10}$	$Q_{100}$	% PRVS	
2.1	2.9	5.1	100%	3.4	5.9	50%	
1.1					3.2		
(Offsite)							

## **CONCLUSION**

The water quality is mitigated thru use of a Modular Wetland System for the project.

House pads are set with minimum elevation of 1 ft above 100 yr flood level, thus providing adequate flood protection for residential pads.

## **SOFTWARE**

We used Software from CivilCADD/Civil Design based on the 1978 Hydrology Manual of RCFC&WCD.

### **RAINFALL**

Rainfall Data for project area is based on Plate D-4.1

10 yr 1hour rainfall 0.94 in 100 yr 1hour rainfall 1.45 in

## **SOIL**

Plate C-1.14 of the RCFC&WCD Hydrology Manual(attached) show hydrological soil group for this project as type "B"

# **Rational Method**

Pre-development

10-year

100-year

```
CIVILCADD/CIVILDESIGN Engineering Software,(c) 1989 - 1999 Version 6.2
    Rational Hydrology Study Date: 04/06/23 File:3360pre10.out
______
TTM36864
PreDev10Yr
     ______
          Hydrology Study Control Information ********
English (in-lb) Units used in input data file
Sake Consulting Engineers, inc., Corona, CA - S/N 4084
______
Rational Method Hydrology Program based on
Riverside County Flood Control & Water Conservation District
1978 hydrology manual
Storm event (year) = 10.00 Antecedent Moisture Condition = 2
Standard intensity-duration curves data (Plate D-4.1)
For the [ Corona ] area used.
10 year storm 10 minute intensity = 2.220(In/Hr)
10 year storm 60 minute intensity = 0.940(In/Hr)
100 year storm 10 minute intensity = 3.430(In/Hr)
100 year storm 60 minute intensity = 1.450(In/Hr)
Storm event year = 10.0
Calculated rainfall intensity data:
1 hour intensity = 0.940(In/Hr)
Slope of intensity duration curve = 0.4800
Process from Point/Station
                           1.000 to Point/Station
**** INITIAL AREA EVALUATION ****
Initial area flow distance = 700.000(Ft.)
Top (of initial area) elevation = 619.000(Ft.)
Bottom (of initial area) elevation = 600.000(Ft.)
Difference in elevation = 19.000(Ft.)
Slope = 0.02714 s(percent)=
TC = k(0.530)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration = 14.982 min.
Rainfall intensity = 1.830(In/Hr) for a 10.0 year storm
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.747
```

IN3360 PreDev10Yr Page 1

```
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 1.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2) = 78.00
Pervious area fraction = 1.000; Impervious fraction = 0.000
Initial subarea runoff =
                              2.868(CFS)
Total initial stream area =
                                   2.100(Ac.)
Pervious area fraction = 1.000
                                                   2.10 (Ac.)
End of computations, total study area =
The following figures may
be used for a unit hydrograph study of the same area.
Area averaged pervious area fraction(Ap) = 1.000
Area averaged RI index number = 78.0
```

JN3360 PreDev10Yr Page 2

```
CIVILCADD/CIVILDESIGN Engineering Software,(c) 1989 - 1999 Version 6.2
    Rational Hydrology Study Date: 04/06/23 File:3360pre.out
______
TTM36864
PreDev100yr
    ______
          Hydrology Study Control Information ********
English (in-lb) Units used in input data file
Sake Consulting Engineers, inc., Corona, CA - S/N 4084
______
Rational Method Hydrology Program based on
Riverside County Flood Control & Water Conservation District
1978 hydrology manual
Storm event (year) = 100.00 Antecedent Moisture Condition = 3
Standard intensity-duration curves data (Plate D-4.1)
For the [ Corona ] area used.
10 year storm 10 minute intensity = 2.220(In/Hr)
10 year storm 60 minute intensity = 0.940(In/Hr)
100 year storm 10 minute intensity = 3.430(In/Hr)
100 year storm 60 minute intensity = 1.450(In/Hr)
Storm event year = 100.0
Calculated rainfall intensity data:
1 hour intensity = 1.450(In/Hr)
Slope of intensity duration curve = 0.4800
Process from Point/Station
                           1.000 to Point/Station
**** INITIAL AREA EVALUATION ****
Initial area flow distance = 700.000(Ft.)
Top (of initial area) elevation = 619.000(Ft.)
Bottom (of initial area) elevation = 600.000(Ft.)
Difference in elevation = 19.000(Ft.)
Slope = 0.02714 s(percent)=
TC = k(0.530)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration = 14.982 min.
Rainfall intensity = 2.822(In/Hr) for a 100.0 year storm
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.854
```

```
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 1.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 3) = 89.80
Pervious area fraction = 1.000; Impervious fraction = 0.000
Initial subarea runoff =
                            5.062(CFS)
Total initial stream area =
                                   2.100(Ac.)
Pervious area fraction = 1.000
                                                   2.10 (Ac.)
End of computations, total study area =
The following figures may
be used for a unit hydrograph study of the same area.
Area averaged pervious area fraction(Ap) = 1.000
Area averaged RI index number = 78.0
```

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# **Rational Method**

Post-development

10-year

100-year

#### Riverside County Rational Hydrology Program

```
CIVILCADD/CIVILDESIGN Engineering Software,(c) 1989 - 1999 Version 6.2
    Rational Hydrology Study Date: 04/06/23 File:3360post10.out
______
TTM36864
PostDev10Yr
     ______
          Hydrology Study Control Information ********
English (in-lb) Units used in input data file
Sake Consulting Engineers, inc., Corona, CA - S/N 4084
______
Rational Method Hydrology Program based on
Riverside County Flood Control & Water Conservation District
1978 hydrology manual
Storm event (year) = 10.00 Antecedent Moisture Condition = 2
Standard intensity-duration curves data (Plate D-4.1)
For the [ Corona ] area used.
10 year storm 10 minute intensity = 2.220(In/Hr)
10 year storm 60 minute intensity = 0.940(In/Hr)
100 year storm 10 minute intensity = 3.430(In/Hr)
100 year storm 60 minute intensity = 1.450(In/Hr)
Storm event year = 10.0
Calculated rainfall intensity data:
1 hour intensity = 0.940(In/Hr)
Slope of intensity duration curve = 0.4800
Process from Point/Station
                           1.000 to Point/Station
**** INITIAL AREA EVALUATION ****
Initial area flow distance = 660.000(Ft.)
Top (of initial area) elevation = 619.000(Ft.)
Bottom (of initial area) elevation = 600.000(Ft.)
Difference in elevation = 19.000(Ft.)
Slope = 0.02879 s(percent)=
TC = k(0.390)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration = 10.642 min.
Rainfall intensity = 2.156(In/Hr) for a 10.0 year storm
SINGLE FAMILY (1/4 Acre Lot)
Runoff Coefficient = 0.753
```

```
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 1.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2) = 56.00
Pervious area fraction = 0.500; Impervious fraction = 0.500
Initial subarea runoff =
                            3.409(CFS)
Total initial stream area =
                                   2.100(Ac.)
Pervious area fraction = 0.500
                                                   2.10 (Ac.)
End of computations, total study area =
The following figures may
be used for a unit hydrograph study of the same area.
Area averaged pervious area fraction(Ap) = 0.500
Area averaged RI index number = 56.0
```

JN3360 PostDev10Yr Page 2

```
CIVILCADD/CIVILDESIGN Engineering Software,(c) 1989 - 1999 Version 6.2
    Rational Hydrology Study Date: 04/06/23 File:3360post.out
______
TTM36864
PostDev100Yr
      ______
          Hydrology Study Control Information ********
English (in-lb) Units used in input data file
Sake Consulting Engineers, inc., Corona, CA - S/N 4084
______
Rational Method Hydrology Program based on
Riverside County Flood Control & Water Conservation District
1978 hydrology manual
Storm event (year) = 100.00 Antecedent Moisture Condition = 3
Standard intensity-duration curves data (Plate D-4.1)
For the [ Corona ] area used.
10 year storm 10 minute intensity = 2.220(In/Hr)
10 year storm 60 minute intensity = 0.940(In/Hr)
100 year storm 10 minute intensity = 3.430(In/Hr)
100 year storm 60 minute intensity = 1.450(In/Hr)
Storm event year = 100.0
Calculated rainfall intensity data:
1 hour intensity = 1.450(In/Hr)
Slope of intensity duration curve = 0.4800
Process from Point/Station
                            1.000 to Point/Station
**** INITIAL AREA EVALUATION ****
Initial area flow distance = 660.000(Ft.)
Top (of initial area) elevation = 619.000(Ft.)
Bottom (of initial area) elevation = 600.000(Ft.)
Difference in elevation = 19.000(Ft.)
Slope = 0.02879 s(percent)=
TC = k(0.390)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration = 10.642 min.
Rainfall intensity = 3.326(In/Hr) for a 100.0 year storm
SINGLE FAMILY (1/4 Acre Lot)
Runoff Coefficient = 0.846
```

```
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 1.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 3) = 74.80
Pervious area fraction = 0.500; Impervious fraction = 0.500
Initial subarea runoff =
                             5.912(CFS)
Total initial stream area =
                                   2.100(Ac.)
Pervious area fraction = 0.500
                                                   2.10 (Ac.)
End of computations, total study area =
The following figures may
be used for a unit hydrograph study of the same area.
Area averaged pervious area fraction(Ap) = 0.500
Area averaged RI index number = 56.0
```

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# **Rational Method**

Off site

100-year

#### Riverside County Rational Hydrology Program

```
CIVILCADD/CIVILDESIGN Engineering Software,(c) 1989 - 1999 Version 6.2
    Rational Hydrology Study Date: 04/06/23 File:3360off10.out
______
TTM36864
Offsite10yr
     ______
          Hydrology Study Control Information ********
English (in-lb) Units used in input data file
Sake Consulting Engineers, inc., Corona, CA - S/N 4084
______
Rational Method Hydrology Program based on
Riverside County Flood Control & Water Conservation District
1978 hydrology manual
Storm event (year) = 10.00 Antecedent Moisture Condition = 2
Standard intensity-duration curves data (Plate D-4.1)
For the [ Corona ] area used.
10 year storm 10 minute intensity = 2.220(In/Hr)
10 year storm 60 minute intensity = 0.940(In/Hr)
100 year storm 10 minute intensity = 3.430(In/Hr)
100 year storm 60 minute intensity = 1.450(In/Hr)
Storm event year = 10.0
Calculated rainfall intensity data:
1 hour intensity = 0.940(In/Hr)
Slope of intensity duration curve = 0.4800
Process from Point/Station
                            1.000 to Point/Station
**** INITIAL AREA EVALUATION ****
Initial area flow distance = 640.000(Ft.)
Top (of initial area) elevation = 645.000(Ft.)
Bottom (of initial area) elevation = 605.000(Ft.)
Difference in elevation = 40.000(Ft.)
Slope = 0.06250 \text{ s(percent)}=
TC = k(0.530)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration = 12.234 min.
Rainfall intensity = 2.017(In/Hr) for a 10.0 year storm
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.759
```

```
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 1.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2) = 78.00
Pervious area fraction = 1.000; Impervious fraction = 0.000
Initial subarea runoff =
                              1.836(CFS)
Total initial stream area =
                                   1.200(Ac.)
Pervious area fraction = 1.000
                                                   1.20 (Ac.)
End of computations, total study area =
The following figures may
be used for a unit hydrograph study of the same area.
Area averaged pervious area fraction(Ap) = 1.000
Area averaged RI index number = 78.0
```

JN3360 Offsite10Yr Page 2

```
CIVILCADD/CIVILDESIGN Engineering Software, (c) 1989 - 1999 Version 6.2
    Rational Hydrology Study Date: 06/21/21 File:33600FF.out
 ______
****** Hydrology Study Control Information *******
English (in-lb) Units used in input data file
Sake Consulting Engineers, inc., Corona, CA
                                        - S/N 4084
______
Rational Method Hydrology Program based on
Riverside County Flood Control & Water Conservation District
1978 hydrology manual
Storm event (year) = 100.00 Antecedent Moisture Condition = 3
Standard intensity-duration curves data (Plate D-4.1)
For the [ Corona ] area used.
10 year storm 10 minute intensity = 2.220(In/Hr)
10 year storm 60 minute intensity = 0.940(In/Hr)
100 year storm 10 minute intensity = 3.430(In/Hr)
100 year storm 60 minute intensity = 1.450(In/Hr)
Storm event year = 100.0
Calculated rainfall intensity data:
1 hour intensity = 1.450(In/Hr)
Slope of intensity duration curve = 0.4800
Process from Point/Station
                             1.000 to Point/Station
                                                        2.000
**** INITIAL AREA EVALUATION ****
Initial area flow distance = 640.000(Ft.)
Top (of initial area) elevation = 645.000(Ft.)
Bottom (of initial area) elevation = 605.000(Ft.)
Difference in elevation = 40.000(Ft.)
Slope = 0.06250 s(percent)=
TC = k(0.530)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration = 12.234 min.
Rainfall intensity =
                      3.111(In/Hr) for a 100.0 year storm
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.858
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 1.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 3) = 89.80
```

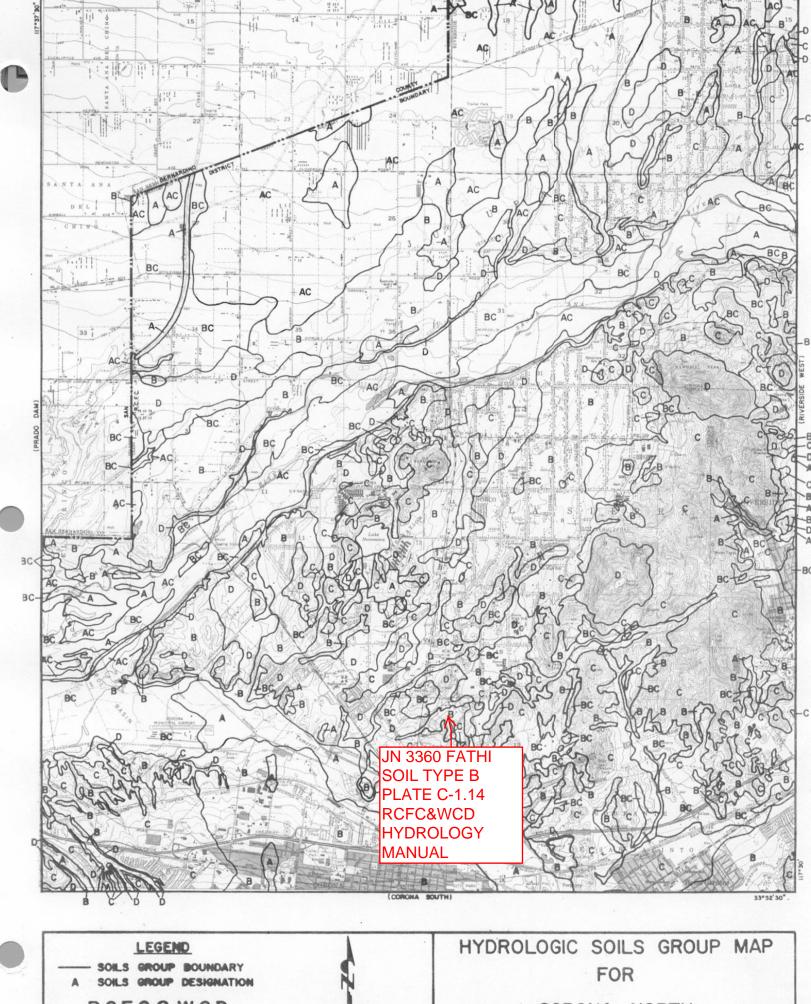
```
Pervious area fraction = 1.000; Impervious fraction = 0.000
Initial subarea runoff = 3.203(CFS)
Total initial stream area = 1.200(Ac.)
Pervious area fraction = 1.000
End of computations, total study area = 1.20 (Ac.)
The following figures may
be used for a unit hydrograph study of the same area.

Area averaged pervious area fraction(Ap) = 1.000
Area averaged RI index number = 78.0
```

Jn3360 Offsite100Yr Page 2

## **EXHIBITS:**

Rainfall for Corona NOAA Atlas 14
Soil Map Plate C-1.14
Pre-development Hydrology Map
Post-development Hydrology Map



RCFC&WCD HYDROLOGY MANUAL



CORONA-NORTH



NOAA Atlas 14, Volume 6, Version 2 Location name: Corona, California, USA\* Latitude: 33.8905°, Longitude: -117.5567° Elevation: m/ft\*\*

source: ESRI Maps
\*\* source: USGS



#### POINT PRECIPITATION FREQUENCY ESTIMATES

Sanja Perica, Sarah Dietz, Sarah Heim, Lillian Hiner, Kazungu Maitaria, Deborah Martin, Sandra Pavlovic, Ishani Roy, Carl Trypaluk, Dale Unruh, Fenglin Yan, Michael Yekta, Tan Zhao, Geoffrey Bonnin, Daniel Brewer, Li-Chuan Chen, Tye Parzybok, John Yarchoan

NOAA, National Weather Service, Silver Spring, Maryland

PF tabular | PF graphical | Maps & aerials

#### PF tabular

PDS-based point precipitation frequency estimates with 90% confidence intervals (in inches) <sup>1</sup>												
Duration	Average recurrence interval (years)											
	1	2	5	10	25	50	100	200	500	1000		
5-min	<b>0.099</b> (0.083-0.119)	<b>0.133</b> (0.111-0.161)	<b>0.179</b> (0.149-0.217)	<b>0.218</b> (0.180-0.267)	<b>0.273</b> (0.217-0.345)	<b>0.316</b> (0.246-0.409)	<b>0.361</b> (0.274-0.480)	<b>0.409</b> (0.302-0.560)	<b>0.476</b> (0.336-0.681)	<b>0.530</b> (0.361-0.786		
10-min	<b>0.142</b> (0.118-0.171)	<b>0.191</b> (0.159-0.230)	<b>0.257</b> (0.214-0.311)	<b>0.312</b> (0.258-0.382)	<b>0.391</b> (0.311-0.495)	<b>0.453</b> (0.353-0.587)	<b>0.518</b> (0.393-0.688)	<b>0.587</b> (0.433-0.803)	<b>0.683</b> (0.482-0.976)	<b>0.760</b> (0.518-1.13)		
15-min	<b>0.171</b> (0.143-0.207)	<b>0.230</b> (0.192-0.279)	<b>0.311</b> (0.259-0.377)	<b>0.378</b> (0.312-0.462)	<b>0.472</b> (0.377-0.599)	<b>0.548</b> (0.427-0.709)	<b>0.626</b> (0.476-0.832)	<b>0.709</b> (0.523-0.971)	<b>0.826</b> (0.583-1.18)	<b>0.919</b> (0.626-1.36		
30-min	<b>0.252</b> (0.211-0.304)	<b>0.339</b> (0.283-0.410)	<b>0.457</b> (0.380-0.554)	<b>0.556</b> (0.459-0.680)	<b>0.695</b> (0.554-0.880)	<b>0.805</b> (0.628-1.04)	<b>0.921</b> (0.700-1.22)	<b>1.04</b> (0.770-1.43)	<b>1.21</b> (0.858-1.74)	<b>1.35</b> (0.921-2.00)		
60-min	<b>0.373</b> (0.312-0.451)	<b>0.502</b> (0.419-0.607)	<b>0.677</b> (0.564-0.821)	<b>0.823</b> (0.680-1.01)	<b>1.03</b> (0.821-1.31)	<b>1.19</b> (0.930-1.55)	<b>1.37</b> (1.04-1.81)	<b>1.55</b> (1.14-2.12)	<b>1.80</b> (1.27-2.57)	<b>2.00</b> (1.37-2.97)		
2-hr	<b>0.553</b> (0.462-0.668)	<b>0.736</b> (0.615-0.890)	<b>0.982</b> (0.818-1.19)	<b>1.19</b> (0.979-1.45)	<b>1.47</b> (1.17-1.86)	<b>1.69</b> (1.32-2.19)	<b>1.93</b> (1.46-2.56)	<b>2.17</b> (1.60-2.97)	<b>2.51</b> (1.77-3.58)	<b>2.77</b> (1.89-4.11)		
3-hr	<b>0.684</b> (0.572-0.826)	<b>0.912</b> (0.762-1.10)	<b>1.22</b> (1.01-1.47)	<b>1.47</b> (1.21-1.79)	<b>1.81</b> (1.45-2.30)	<b>2.09</b> (1.63-2.70)	<b>2.37</b> (1.80-3.15)	<b>2.66</b> (1.96-3.64)	<b>3.06</b> (2.16-4.38)	<b>3.38</b> (2.30-5.01)		
6-hr	<b>0.956</b> (0.800-1.16)	<b>1.29</b> (1.08-1.56)	<b>1.74</b> (1.45-2.10)	<b>2.10</b> (1.73-2.57)	<b>2.60</b> (2.07-3.30)	<b>2.99</b> (2.33-3.87)	<b>3.39</b> (2.58-4.51)	<b>3.81</b> (2.81-5.21)	<b>4.37</b> (3.09-6.25)	<b>4.82</b> (3.28-7.14)		
12-hr	<b>1.21</b> (1.01-1.46)	<b>1.71</b> (1.43-2.07)	<b>2.36</b> (1.97-2.86)	<b>2.90</b> (2.39-3.54)	<b>3.62</b> (2.89-4.59)	<b>4.18</b> (3.26-5.42)	<b>4.76</b> (3.62-6.33)	<b>5.35</b> (3.95-7.33)	<b>6.16</b> (4.35-8.81)	<b>6.79</b> (4.63-10.1)		
24-hr	<b>1.57</b> (1.39-1.81)	<b>2.31</b> (2.04-2.67)	<b>3.28</b> (2.89-3.80)	<b>4.07</b> (3.56-4.75)	<b>5.14</b> (4.35-6.20)	<b>5.97</b> (4.95-7.34)	<b>6.81</b> (5.51-8.58)	<b>7.68</b> (6.05-9.94)	<b>8.86</b> (6.70-11.9)	<b>9.78</b> (7.16-13.6)		
2-day	<b>1.99</b> (1.76-2.29)	<b>2.93</b> (2.59-3.38)	<b>4.16</b> (3.67-4.82)	<b>5.17</b> (4.52-6.03)	<b>6.54</b> (5.53-7.88)	<b>7.59</b> (6.30-9.34)	<b>8.66</b> (7.02-10.9)	<b>9.78</b> (7.70-12.7)	<b>11.3</b> (8.54-15.2)	<b>12.5</b> (9.12-17.4)		
3-day	<b>2.19</b> (1.94-2.52)	<b>3.21</b> (2.84-3.71)	<b>4.56</b> (4.01-5.28)	<b>5.65</b> (4.94-6.60)	<b>7.15</b> (6.05-8.62)	<b>8.31</b> (6.89-10.2)	<b>9.49</b> (7.68-12.0)	<b>10.7</b> (8.44-13.9)	<b>12.4</b> (9.36-16.7)	<b>13.7</b> (10.0-19.1)		
4-day	<b>2.39</b> (2.11-2.75)	<b>3.50</b> (3.09-4.04)	<b>4.96</b> (4.37-5.75)	<b>6.16</b> (5.39-7.19)	<b>7.80</b> (6.60-9.40)	<b>9.07</b> (7.52-11.2)	<b>10.4</b> (8.39-13.1)	<b>11.7</b> (9.22-15.2)	<b>13.5</b> (10.2-18.2)	<b>15.0</b> (10.9-20.9)		
7-day	<b>2.75</b> (2.43-3.17)	<b>4.01</b> (3.54-4.63)	<b>5.67</b> (5.00-6.57)	<b>7.04</b> (6.16-8.22)	<b>8.93</b> (7.56-10.8)	<b>10.4</b> (8.62-12.8)	<b>11.9</b> (9.64-15.0)	<b>13.5</b> (10.6-17.4)	<b>15.6</b> (11.8-21.1)	<b>17.3</b> (12.7-24.2)		
10-day	<b>2.97</b> (2.63-3.42)	<b>4.31</b> (3.81-4.97)	<b>6.09</b> (5.37-7.06)	<b>7.57</b> (6.62-8.84)	<b>9.62</b> (8.15-11.6)	<b>11.2</b> (9.31-13.8)	<b>12.9</b> (10.4-16.2)	<b>14.6</b> (11.5-18.9)	<b>17.0</b> (12.9-22.9)	<b>18.9</b> (13.8-26.4)		
20-day	<b>3.56</b> (3.15-4.11)	<b>5.13</b> (4.54-5.93)	<b>7.27</b> (6.41-8.42)	<b>9.07</b> (7.93-10.6)	<b>11.6</b> (9.82-14.0)	<b>13.6</b> (11.3-16.8)	<b>15.7</b> (12.7-19.8)	<b>18.0</b> (14.2-23.3)	<b>21.1</b> (16.0-28.5)	<b>23.6</b> (17.3-32.9)		
30-day	<b>4.22</b> (3.73-4.87)	<b>6.03</b> (5.33-6.97)	<b>8.53</b> (7.52-9.88)	<b>10.7</b> (9.32-12.4)	<b>13.7</b> (11.6-16.5)	<b>16.1</b> (13.4-19.9)	<b>18.7</b> (15.2-23.6)	<b>21.5</b> (16.9-27.8)	<b>25.4</b> (19.2-34.3)	<b>28.6</b> (20.9-39.9)		
45-day	<b>5.03</b> (4.45-5.80)	<b>7.08</b> (6.26-8.18)	<b>9.96</b> (8.77-11.5)	<b>12.4</b> (10.9-14.5)	<b>16.0</b> (13.6-19.3)	<b>19.0</b> (15.7-23.3)	<b>22.1</b> (17.9-27.9)	<b>25.5</b> (20.1-33.0)	<b>30.4</b> (23.0-41.0)	<b>34.5</b> (25.2-48.1)		
60-day	<b>5.82</b> (5.15-6.72)	<b>8.06</b> (7.13-9.31)	<b>11.2</b> (9.90-13.0)	<b>14.0</b> (12.2-16.4)	<b>18.1</b> (15.3-21.8)	<b>21.4</b> (17.8-26.4)	<b>25.1</b> (20.3-31.6)	<b>29.1</b> (22.9-37.6)	<b>34.9</b> (26.4-47.0)	<b>39.7</b> (29.1-55.4)		

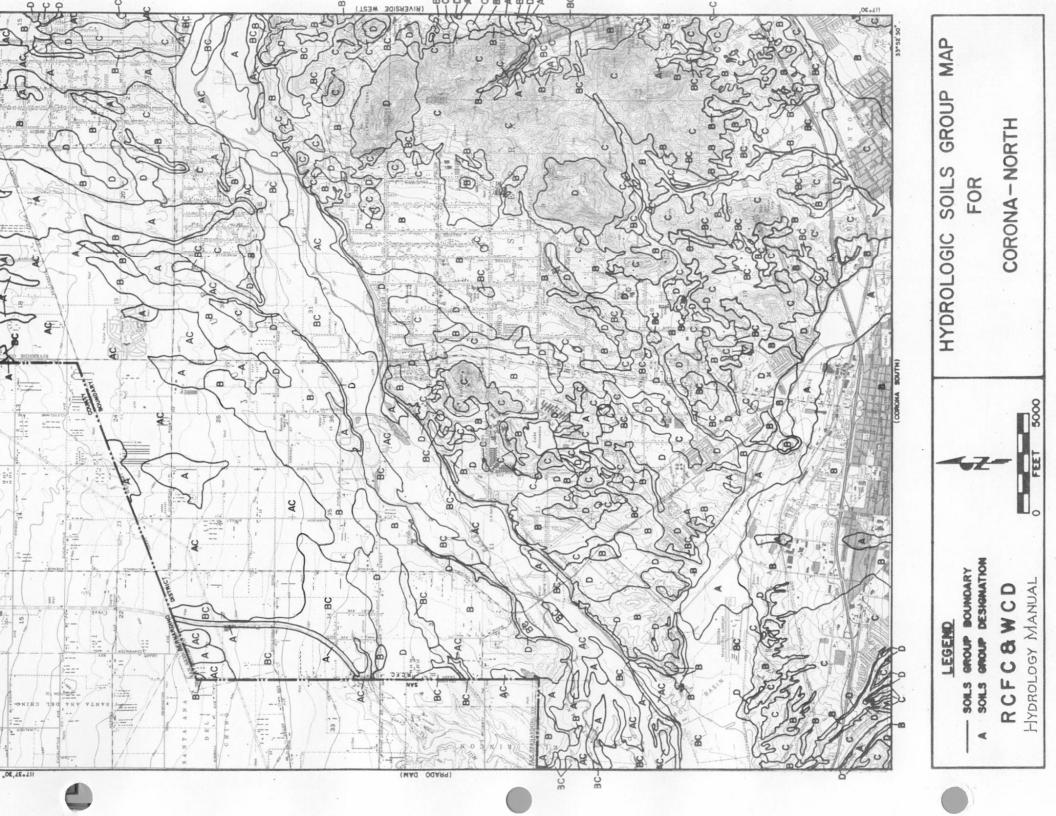
<sup>&</sup>lt;sup>1</sup> Precipitation frequency (PF) estimates in this table are based on frequency analysis of partial duration series (PDS).

Numbers in parenthesis are PF estimates at lower and upper bounds of the 90% confidence interval. The probability that precipitation frequency estimates (for a given duration and average recurrence interval) will be greater than the upper bound (or less than the lower bound) is 5%. Estimates at upper bounds are not checked against probable maximum precipitation (PMP) estimates and may be higher than currently valid PMP values.

Please refer to NOAA Atlas 14 document for more information.

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### PF graphical



## **OWNER/DEVELOPER:**

FATHI MANASRAH, P.E.
AL—WAAFA FAMILY TRUST
9319 ALTA CRESTA AVENUE
RIVERSIDE, CA 92508
TEL. (951) 581—2330

## **ENGINEER:**

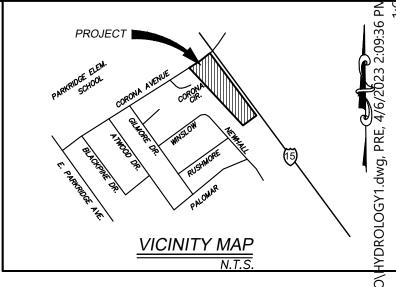
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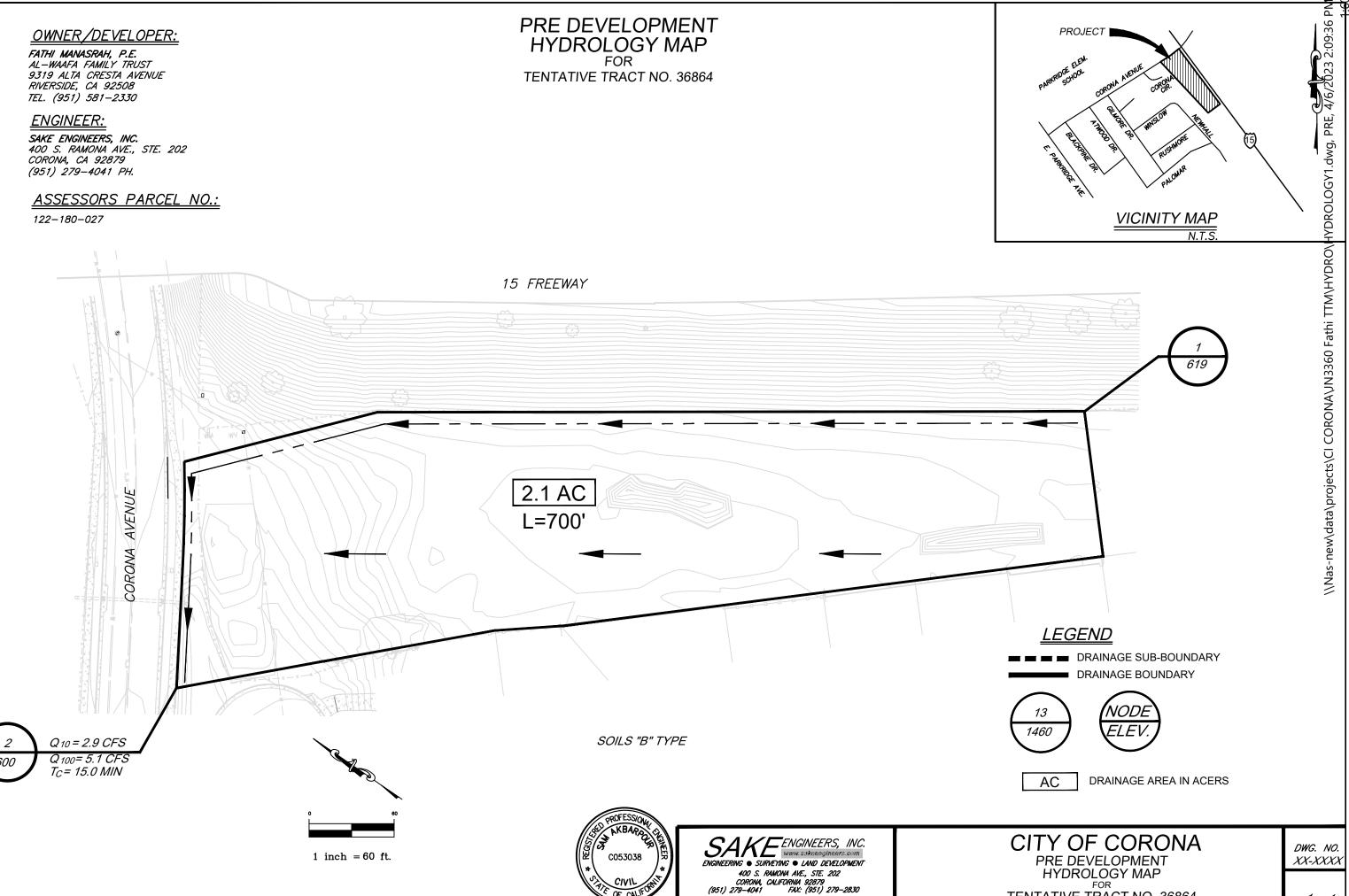
## PRE DEVELOPMENT HYDROLOGY MAP **FOR**

**TENTATIVE TRACT NO. 36864** 



TENTATIVE TRACT NO. 36864

sh 1 of 1



## OWNER/DEVELOPER:

FATHI MANASRAH, P.E.
AL—WAAFA FAMILY TRUST
9319 ALTA CRESTA AVENUE
RIVERSIDE, CA 92508
TEL. (951) 581—2330

## **ENGINEER:**

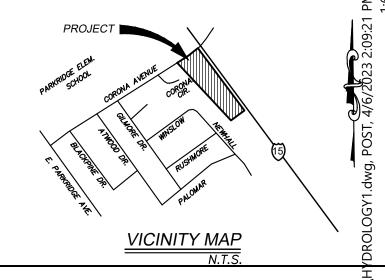
SAKE ENGINEERS, INC. 400 S. RAMONA AVE., STE. 202 CORONA, CA 92879 (951) 279-4041 PH.

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## POST DEVELOPMENT **HYDROLOGY MAP FOR**

**TENTATIVE TRACT NO. 36864** 



sh 1 of 1

